

International Journal of Advance Research in Engineering, Science & Technology

# *e-ISSN: 2393-9877, p-ISSN: 2394-2444 Volume 5, Issue 12, December-2018* Parametric Optimization of Abrasive Water Jet Cutting during Machining of AISI4140 steel

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Abstract — Abrasive water jet Machining (AWJM) is one of the widely used non-traditional machining process. It is capable of machining geometrically complex and hard material components, that are precise and difficult-to-machine such as heat-treated tool steels, composites, super alloys, ceramics, carbides, heat resistant steels etc. being widely used in die and mould making industries, aerospace, and aeronautics industries. In present study, Experimental investigations were conducted to assess the influence of process parameters like Abrasive mass flow rate(gm/min), traverse speed (mm/min) and Stand of Distance (mm) on Material Removal Rate (mm<sup>3</sup>/min) and Surface Roughness (µm) of AISI 4140 steel. Here, using garnet and Aluminium oxide mixer as an abrasive material. The optimization for Abrasive water jet Machining process parameters of AISI 4140 Steel work piece using Taguchi method will done. Thirty-two experimental runs (L32) based on an orthogonal array Taguchi method will performed and investigate the effect of Abrasive water jet cutting process parameters like Abrasive size (mesh). Abrasive mass Flow Rate (gm/min), Traverse speed (mm/min) and Stand of Distance (mm) on Material Removal rate, Surface Roughness and Kerf width. The MRR, SR and kerf width were measured for each specimen after AWJC and the effects of these parameters were researched.

# Keywords- Abrasive water jet cutting, abrasive size, Pressure, Transverse speed, Stand of Distance, Surface roughness, Material Removal Rate, Kerf width

#### I. INTRODUCTION

Abrasive water jet (AWJ) technology and its applications had been commercialized since long. Since then, significant advances have been made in AWJM in the form of hardware and software integration, abrasive suspension jet machining (ASJM), cryogenic abrasive water jets, super-water jetting, percussive (rapidly pulsing jets) machining, and oscillation pulsed jet along with newer applications in drilling, milling, taper cutting, turning, threading, etc. A wide range of materials (Inconel, Titanium, Incoloy, glass, ceramics, composites, heat-sensitive alloys, etc.) is shaped for different applications with this process. The demand of higher strength and heat resistant material is increasing particularly in aerospace industries. However, these materials are often difficult to machine due to their physical and mechanical properties such as high strength and low thermal conductivity, which requires very high cutting energy and makes the cutting forces and cutting temperature very high, and even leads to a short tool life. [1]



Figure 1 Abrasive water jet machining

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| Sr no | Abrasive size [mesh] | Pressure    | Traverse speed [mm/min]               | in] Sod [mm] |  |  |
|-------|----------------------|-------------|---------------------------------------|--------------|--|--|
|       |                      | [MPa]       |                                       |              |  |  |
| 1     | 80                   | 250         | 50                                    | 2            |  |  |
| 2     | 80                   | 250         | 75                                    | 3            |  |  |
| 3     | 80                   | 250         | 100                                   | 4            |  |  |
| 4     | 80                   | 250         | 125                                   | 5            |  |  |
| 5     | 80                   | 350         | 50                                    | 2            |  |  |
| 6     | 80                   | 350         | 75                                    | 3            |  |  |
| 7     | 80                   | 350         | 100                                   | 4            |  |  |
| 8     | 80                   | 350         | 125                                   | 5            |  |  |
| 9     | 80                   | 450         | 50                                    | 3            |  |  |
| 10    | 80                   | 450         | 75                                    | 2            |  |  |
| 11    | 80                   | 450         | 100                                   | 5            |  |  |
| 12    | 80                   | 450         | 125                                   | 4            |  |  |
| 13    | 80                   | 550         | 50                                    | 3            |  |  |
| 14    | 80                   | 550         | 75                                    | 2            |  |  |
| 15    | 80                   | 550         | 100                                   | 5            |  |  |
| 16    | 80                   | 550         | 125                                   | 4            |  |  |
| 17    | 120                  | 250         | 50                                    | 5            |  |  |
| 18    | 120                  | 250         | 75                                    | 4            |  |  |
| 19    | 120                  | 250         | 100                                   | 3            |  |  |
| 20    | 120                  | 250         | 125                                   | 2            |  |  |
| 21    | 120                  | 350         | 50                                    | 5            |  |  |
| 22    | 120                  | 350         | 75                                    | 4            |  |  |
| 23    | 120                  | 350         | 100                                   | 3            |  |  |
| 24    | 120                  | 350         | 125                                   | 2            |  |  |
| 25    | 120                  | 450         | 50                                    | 4            |  |  |
| 26    | 120                  | 450         | 75                                    | 5            |  |  |
| 27    | 120                  | 450         | 100                                   | 2            |  |  |
| 28    | 120                  | 450         | 125                                   | 3            |  |  |
| 29    | 120                  | 550         | 50                                    | 4            |  |  |
| 30    | 120                  | 550         | 75                                    | 5            |  |  |
| 31    | 120                  | 550         | 100                                   | 2            |  |  |
| 32    | 120                  | 550         | 125                                   | 3            |  |  |
|       | •                    | · · · · · · | · · · · · · · · · · · · · · · · · · · |              |  |  |

Table 1 Orthogonal array Taguchi L32

#### III. Analysis of Variance (ANOVA)

Above analysis shows the percentage contribution of individual parameters on surface roughness. The percentage contribution of is Abrasive size 8.5 %, Pressure is 59.3 %, Transverse rate is 28.9 % and Sod is 0.2 %. And error is 3.07 %. this error is due to human ineffectiveness.

Above analysis shows the percentage contribution of individual parameters on MRR. The percentage contribution of is Abrasive size5.9 %, Pressure is 30.8 %, Transverse rate is 50.4% and Sod is 0.6 %. And error is 12.27 %. this error is due to human ineffectiveness.

Above analysis shows the percentage contribution of individual parameters on Top kerf width. The percentage contribution of is Abrasive size 15.5 %, Pressure is 25.9 %, Transverse rate is 49.1 % and Sod is 1.1 %. And error is 8.4 %. this error is due to human ineffectiveness.

Above analysis shows the percentage contribution of individual parameters on Bottom kerf width. The percentage contribution of is Abrasive size1.0 %, Pressure is 61.4 %, Transverse rate is 20.3 % and Sod is 3.0 %. And error is 14.24 %. this error is due to human ineffectiveness.

#### IV. REGRESSION ANALYSIS

Top Kerf Width = 0.508 + 0.000828(Abrasive size) + 0.000191(Pressure) + 0.00105 (Traverse Speed) - 0.00338(SOD) Bottom Kerf Width = 0.451 + 0.000250 (Abrasive size) + 0.000307(Pressure) + 0.000670 (Traverse Speed) + 0.00775(SOD)

| V.   | <b>)</b> ptimization methodology using grey relational analysis |
|------|---|
| Tabl | Crew relational coefficient and area relational grade values    |

| Tuble 2 Grey relational coefficient and grey relational grade values |                      |                             |                      |                         |                           |                             |                      |                         |                     |      |
|--|----------------------|-----------------------------|----------------------|-------------------------|---------------------------|-----------------------------|----------------------|-------------------------|---------------------|------|
|  | deviation sequence   |                             |                      |                         | Grey Relation Coefficient |                             |                      |                         |                     |      |
| Run No.  | Surface<br>Roughness | Material<br>Removal<br>Rate | Top<br>Kerf<br>Width | bottom<br>kerf<br>width | Surface<br>Roughness      | Material<br>Removal<br>Rate | Top<br>Kerf<br>Width | bottom<br>kerf<br>width | grey relation grade | rank |
| 1  | 0.43                 | 0.76                        | 0.00                 | 0.00                    | 0.538                     | 0.395                       | 1.000                | 1.000                   | 0.298               | 29   |
| 2  | 0.26                 | 0.73                        | 0.00                 | 0.15                    | 0.656                     | 0.408                       | 1.000                | 0.769                   | 0.284               | 30   |
| 3  | 0.19                 | 0.51                        | 0.12                 | 0.30                    | 0.724                     | 0.493                       | 0.810                | 0.625                   | 0.281               | 32   |
| 4  | 0.07                 | 0.37                        | 0.24                 | 0.45                    | 0.875                     | 0.576                       | 0.680                | 0.526                   | 0.281               | 31   |

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| 5  | 0.74 | 0.57 | 0.00 | 0.10 | 0.404 | 0.467 | 1.000 | 0.833 | 0.352 | 27 |
|----|------|------|------|------|-------|-------|-------|-------|-------|----|
| 6  | 0.67 | 0.37 | 0.18 | 0.25 | 0.429 | 0.576 | 0.739 | 0.667 | 0.365 | 26 |
| 7  | 0.57 | 0.29 | 0.41 | 0.50 | 0.467 | 0.636 | 0.548 | 0.500 | 0.442 | 18 |
| 8  | 0.43 | 0.23 | 0.59 | 0.65 | 0.538 | 0.690 | 0.459 | 0.435 | 0.473 | 15 |
| 9  | 0.95 | 0.79 | 0.18 | 0.45 | 0.344 | 0.387 | 0.739 | 0.526 | 0.593 | 5  |
| 10 | 0.86 | 0.37 | 0.35 | 0.55 | 0.368 | 0.576 | 0.586 | 0.476 | 0.532 | 12 |
| 11 | 0.69 | 0.17 | 0.41 | 0.75 | 0.420 | 0.749 | 0.548 | 0.400 | 0.505 | 14 |
| 12 | 0.50 | 0.08 | 0.59 | 0.65 | 0.500 | 0.859 | 0.459 | 0.435 | 0.455 | 17 |
| 13 | 1.00 | 0.41 | 0.24 | 0.55 | 0.333 | 0.551 | 0.680 | 0.476 | 0.548 | 8  |
| 14 | 0.90 | 0.29 | 0.41 | 0.55 | 0.356 | 0.636 | 0.548 | 0.476 | 0.538 | 9  |
| 15 | 0.76 | 0.29 | 0.47 | 0.75 | 0.396 | 0.631 | 0.515 | 0.400 | 0.569 | 7  |
| 16 | 0.62 | 0.08 | 0.65 | 0.80 | 0.447 | 0.864 | 0.436 | 0.385 | 0.536 | 10 |
| 17 | 0.26 | 1.00 | 0.24 | 0.25 | 0.656 | 0.333 | 0.680 | 0.667 | 0.437 | 20 |
| 18 | 0.19 | 0.87 | 0.29 | 0.15 | 0.724 | 0.365 | 0.630 | 0.769 | 0.377 | 25 |
| 19 | 0.12 | 0.61 | 0.35 | 0.30 | 0.808 | 0.450 | 0.586 | 0.625 | 0.346 | 28 |
| 20 | 0.00 | 0.62 | 0.59 | 0.45 | 1.000 | 0.447 | 0.459 | 0.526 | 0.414 | 23 |
| 21 | 0.67 | 0.97 | 0.06 | 0.05 | 0.429 | 0.341 | 0.895 | 0.909 | 0.436 | 21 |
| 22 | 0.57 | 0.65 | 0.24 | 0.15 | 0.467 | 0.435 | 0.680 | 0.769 | 0.402 | 24 |
| 23 | 0.29 | 0.37 | 0.65 | 0.45 | 0.636 | 0.576 | 0.436 | 0.526 | 0.438 | 19 |
| 24 | 0.31 | 0.33 | 0.71 | 0.50 | 0.618 | 0.603 | 0.415 | 0.500 | 0.461 | 16 |
| 25 | 0.88 | 0.80 | 0.24 | 0.55 | 0.362 | 0.385 | 0.680 | 0.476 | 0.617 | 3  |
| 26 | 0.69 | 0.40 | 0.41 | 0.80 | 0.420 | 0.558 | 0.548 | 0.385 | 0.575 | 6  |
| 27 | 0.50 | 0.21 | 0.65 | 0.75 | 0.500 | 0.700 | 0.436 | 0.400 | 0.528 | 13 |
| 28 | 0.33 | 0.00 | 0.71 | 0.70 | 0.600 | 1.000 | 0.415 | 0.417 | 0.435 | 22 |
| 29 | 0.74 | 0.54 | 0.41 | 0.85 | 0.404 | 0.481 | 0.548 | 0.370 | 0.635 | 2  |
| 30 | 0.69 | 0.38 | 0.65 | 0.75 | 0.420 | 0.571 | 0.436 | 0.400 | 0.616 | 4  |
| 31 | 0.52 | 0.29 | 0.76 | 0.55 | 0.488 | 0.631 | 0.395 | 0.476 | 0.533 | 11 |
| 32 | 0.40 | 0.27 | 1.00 | 1 00 | 0 553 | 0.651 | 0 333 | 0 333 | 0.668 | 1  |



Figure 2Main effect plot of grey relational grade

#### VI. Conclusion

- > Traverse speed is most critical variable for MRR and SR contrasted with different parameters.
- Increase of traverse speed produces more start vitality as the abrasive flow rate that the MRR rise and SR diminishes with traverse speed. Abrasive flow rate is most critical parameter in all outputs. Surface roughness likewise increments with increment of abrasive size on the grounds that the increments of abrasive size create hole with more extensive and more profound trademark.
- Traverse speed has inverse impact to abrasive size. MRR rises with increment of traverse speed, while surface roughness decreases.
- The MRR diminishes with increment in stand of distance. This is because of increment in stand of distance result in higher release vitality per start as a result of expansive abrasive particle between working crevice; subsequently the MRR diminishes.

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